



An occultation experiment is a promising method for retrieving aerosol vertical profile in the stratosphere. In this case, radiation attenuated by the long atmospheric paths is registered from space at starset.

An equation for radiation transfer for occultation geometry is rather simple:

$$(1) \quad I_{\lambda}(h) = I_{\lambda}^*(h)$$

Here  $I_{\lambda}(h)$  is the radiation registered along the viewing line with its pedigree altitude,  $h$ ;  $I_{\lambda}^*$  is the intensity of the extra atmospheric solar radiation. The atmospheric optical thickness  $\tau_{\lambda}(h)$  along the viewing line is calculated by the formula:

$$(2) \quad \tau_{\lambda}(h) = \exp \left\{ -2 \int_h^{\infty} (\beta_{\lambda}(h') dx(h, h')) \right\},$$

where  $(\beta_{\lambda}(h))$  is an unknown distribution of the attenuation coefficient with an altitude  $h$ ;  $x(h, h')$  in the variable of the geometrical part along the viewing line between the points at altitudes  $h$  and  $h'$ .

It is seen from the above two equations that the solution of the inverse problem is reduced to solution for  $\beta(h')$  in the Volterra's equation of the first kind:

$$(3) \quad g_{\lambda}(h) = \ln \{ 1 / \tau_{\lambda}(h) \} = 2 \int_h^{\infty} \beta(h') dx(h, h'),$$

The star occultation geometry (fig. 1) is typically used to measure the stratosphere because of clouds in the troposphere. The extinction by clouds is so high that the attenuation of the radiation by aerosols would be undetectable.

In the case of the "occultation-mode" the radiative transfer is completely described by the law of extinction (4), which is the analytical solution of the appropriate special case of the equation of radiative transfer and which is simple compared to the "scattering-mode":

$$(4) \quad E_{\lambda} = E_{\Theta\lambda} \exp - (\delta_{R\lambda} + \delta_{G\lambda} + \delta_{D\lambda}),$$

Where:

- $E$  – spectral solar flux density at the spectrometer;
- $E_{\Theta\lambda}$  – spectral solar flux density before entering the atmosphere;
- $\delta_{R\lambda}$  – optical depth of the atmosphere integrated over the optical path, due to air molecules (Rayleigh optical depth);
- $\delta_{G\lambda}$  – same, due to absorption by gases;
- $\delta_{D\lambda}$  – same, due to aerosol particles.

As can be seen from (4) the desired quantity, the aerosol optic depth can be gained reasonably by simply "inverting" the measured quantity  $E_{\lambda}$ . In fact the Rayleigh optical depth is the only perturbing quantity. The gaseous absorption on optical depth can be chosen to be zero by an appropriate choice of the peak wavelengths and the bandwidths of the spectrometer channels.

The developed method is provided by an absorption ozonemeter. The absorption ozonemeter consists of the following constructive blocks: hinge block with a position lock pin, lather light-protective blind, vizir, photometric channel and connection cable to the apparatus.

The general view of pulse photometer is presented on fig. 2.

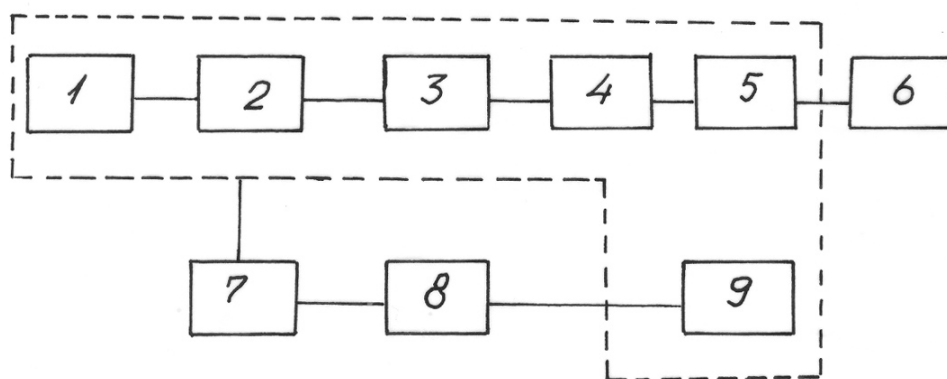


Fig. 2. Block-scheme of absorption ozonometer: 1-sight-protective device; 2-objectives; 3- filter block; 4-sensor; 5-photon counter; 6-microprocessing unit; 7-guiding device; 8-operator; 9-control desk.

The hinge block serves for the absorption ozonometer mounting to the space station illuminator. A lock pin for positioning is assembled in it, which provides fixing of the pulse photometer in the desired direction. The blind serves for photometer objective and vizir protection from side lightings. The vizir serves for apparatus guiding to the researched object.

The photometric channel consists of the following blocks, changeable filters block, input optical system, photometric multiplier, analogue unit, digital unit, control panel. The input optical system means an afocal objective. It serves for receiving of the optical signal, as at its output a concentrated parallel beam which descends on the corresponding interference filter is formed.

A diaphragm is located in the focal plane.

The design permits the diaphragm shift depending on the required in the experiment visual field. The photo electronic multiplier is provided for the information flow conversion into electronic signal. The used photoelectric multiplier is of 9893 B/100 type, made by "Torn EMI". A secondary supplying source for stabilized voltages ( $\pm 15$  V, 5 V, +1,5 V, ...2,3 kV, 27 V) is provided. The analogue unit serves for signal amplification and forming into convenient shape for digital conversion at the input of the photoelectric multiplier. The digital unit is provided for solving of following tasks: counting of pulses from analogue unit, signal transmission for recording in apparatus, run mode of absorption ozonometer selection, providing of control panel indication.

The changeable filters block provides the subsequent transition of the photon flux trough the various interference filters to the photoelectric multiplier. The control panel serves for: switching on the power supply of absorption ozonometer, selection of automatic or manual mode of filter change, selection of high time resolution mode "100  $\mu$ s" or low time resolution mode "1 ms" and "100 ms", manual selection of the desired filters, switching on the mode of the information recording into the apparatus.

Run mode of absorption ozonometer.

The light flux from the researched object is registered by the following sequence: transmitting trough the optical system and filter block, it hits the photocathode of the photoelectric multiplier anode the signals pass in the form of electrical pulses to the analogue unit where they are amplified into digital form.

Depending on the selector position "100  $\mu$ s – 1 ms – 100 ms" on the control panel, the digital unit counts this pulses with high (100  $\mu$ s) or low (1 ms or 100 ms) time resolution.

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